# Subwavelength Gold Grating as Polarizers Integrated with InP-Based InGaAs Sensors 

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#### Abstract

There are currently growing needs for polarimetric imaging in infrared wavelengths for broad applications in bioscience, communications and agriculture, etc. Subwavelength metallic gratings are capable of separating transverse magnetic (TM) mode from transverse electric (TE) mode to form polarized light, offering a reliable approach for the detection in polarization way. This work aims to design and fabricate subwavelength gold gratings as polarizers for InP-based InGaAs sensors in $1.0-1.6 \mu \mathrm{~m}$. The polarization capability of gold  gratings on InP substrate with pitches in the range of 200-1200 nm (fixed duty cycle of 0.5 ) has been systematically studied by both theoretical modeling with a finite-difference time-domain (FDTD) simulator and spectral measurements. Gratings with 200 nm lines/space in 100 -nm-thick gold have been fabricated by electron beam lithography (EBL). It was found that subwavelength gold gratings directly integrated on InP cannot be applied as good polarizers, because of the existence of SPP modes in the detection wavelengths. An effective solution has been found by sandwiching the $\mathrm{Au} / \mathrm{InP}$ bilayer using a 200 nm SiO extinction ratio. At $1.35 \mu \mathrm{~m}$, the improvement factors are 8 and 10 , respectively. Therefore, it is concluded that the $\mathrm{Au} / \mathrm{SiO}_{2} / \mathrm{InP}$ trilayer should be a promising candidate of near-infrared polarizers for the InP-based InGaAs sensors.


KEYWORDS: subwavelength gold grating, polarizer, surface plasmon polariton, cavity mode, InP-based InGaAs sensor

## 1. INTRODUCTION

The polarimetric imaging technique provides unique advantages in the detection of images with improved contrast and low noise over conventional wavelength ones. Because of this, it has exhibited extensive applications. Notably, in medicine, it can be applied to enhance the contrast between healthy and cancerous zones of colon specimens, in order to facilitate the early detection of cancer. ${ }^{1}$ In environmental protection, it can spot oil-slick-contaminated sea surfaces in slick-free areas. ${ }^{2}$ In biological systems, it was used in mantis shrimp compound eyes to improve underwater sensitivity. ${ }^{3}$ In forensic science, it can improve the efficiency to detect latent fingerprint images. ${ }^{4}$ Traditionally, polarization information is obtained by rotating a linear polarizer in front of the sensor. ${ }^{5,6}$ Stokes parameters are captured at different instants of time, leading to the artifacts in polarimetric imaging, especially for fast moving targets. ${ }^{7}$ To eliminate these defects, division of focal plane (DoFP) is introduced by monolithically integrating pixelated micropolarizers of different orientations onto the sensor, to obtain instantaneous Stokes parameters. ${ }^{8-10}$

It has been well-known that a subwavelength metallic grating (SMG) has the function of polarization, in which transverse magnetic (TM) mode is transmitted and transverse electric (TE) mode is blocked for a light impinging onto it. ${ }^{11-17}$ Compared with crystal and polymer polarizer, SMG has the advantages of miniaturized dimensions, high spatial resolution, and good temperature tolerance, which is beneficial for highly pixelated match requirement in DoFP polarimetric imaging. ${ }^{18}$ InGaAs material with lattice matched InP substrate has been widely used in the field of astronomical detection, Earth observation, and machine vision. ${ }^{19-21}$ SMG has been integrated onto CCD/CMOS to prove the feasibility in the visible range. ${ }^{18,22-24}$ However, the integration of SMG onto shortwave infrared (SWIR) InGaAs sensor has yet been reported so far.

[^0]In this work, we proposed to integrate a subwavelength gold grating (SGG) as a polarizer to InP-based InGaAs sensors for the application in polarization detection in $1.0-1.6 \mu \mathrm{~m}$. However, it was discovered that SGG with a pitch of 200500 nm cannot fully functionalize as a polarizer, because of the existence of SPP resonance. This problem was successfully solved by inserting a 200 nm SiO 2 layer into the $\mathrm{Au} / \mathrm{InP}$ interface. Nanofabrication of SGG polarizers was fabricated by electron beam lithography (EBL). The polarization property of the fabricated SGG has been carefully characterized by both numerical simulation and optical measurements, demonstrating its promising future in the application of InP-based InGaAs detector for polarimetric imaging.

## 2. EXPERIMENTAL SECTION

Fabrication of SGG Polarizers. For comparison, 200 nm lines/ space gold gratings were fabricated on InP and $\mathrm{SiO}_{2} / \mathrm{InP}$, respectively, by EBL, followed by gold thermal deposition and lift-off in acetone. The grating area is $2 \mathrm{~mm} \times 2 \mathrm{~mm}$, and the gold thickness is 100 nm . In the EBL, a positive tone UVIII was first spin-coated on InP substrate at 4000 rpm for 60 s for a thickness of $\sim 600 \mathrm{~nm}$, then baked at $130^{\circ} \mathrm{C}$ for 60 s immediately. A state-of-the-art beam writer (Model JBX-6300FS, JEOL) was used for e-beam exposure, followed by postexposure bake at $130^{\circ} \mathrm{C}$ for 90 s. The exposed resist was subsequently developed by CD26 at $23{ }^{\circ} \mathrm{C}$ for 60 s , and finally rinsed in deionized water (DIW) for 30 s . On this basis, $10 \mathrm{~nm} \mathrm{Cr} / 100 \mathrm{~nm}$ gold was deposited using thermal evaporation with NANO36 (Kurt J. Lesker). The process was completed by a lift-off in acetone. Figure 1 presents a micrograph by scanning electron microscopy (SEM) for the fabricated gold grating.


Figure 1. A SEM micrograph for the fabricated subwavelength gold grating (SGG) on a InP substrate.

Optical Measurement. Two optical systems, as schematically shown in Figure 2, were built to measure the transmission of SGG polarizers. For the measurement of normal transmission spectrum in the range of $1.0-1.6 \mu \mathrm{~m}$, a tungsten-halogen lamp was used (Figure 2a). After passing through a commercial polarizer, the sample, and a grating spectrometer in sequence, the emergent light was received by an InGaAs sensor. For angle-resolved transmission spectra, a solidstate laser (wavelength $=1342 \mathrm{~nm}$, beam diameter $=1.5 \mathrm{~mm}$ ) was used as a light source, followed by a neutral density filter, a quarterwave plate, and a Glan-Thompson polarizer (Figure 2b). The laser beam was confined by using a $1 \mathrm{~mm} \times 1 \mathrm{~mm}$ diaphragm. Both the sample and the diaphragm were fixed on a rotational stage by which the incident angle was changed in the range of $0-35^{\circ}$. All


Figure 2. Schematics of optical measurement systems: (a) normal transmission spectrum in the range of $1.0-1.6 \mu \mathrm{~m}$ and (b) angleresolved transmission spectrum at 1342 nm .
measurements were carried out at room temperature. The measured data were smoothed by fast Fourier transform (FFT).

## 3. RESULTS AND DISCUSSION

In this section, polarization property of SGG on InP and $\mathrm{SiO}_{2} /$ $\operatorname{InP}$, respectively, are investigated by both theoretically modeling and optical measurement.

SGG Polarizer on InP. The transmission spectra of SGG on InP were first calculated using the FDTD algorithm ${ }^{25}$ with commercial software delivered by Lumerical, Ltd. To gain insight of the transmission mechanism, electric field distributions and the Poynting vector were also computed. The frequency-dependent dielectric constant functions of gold and InP were fitted by multicoefficient models (MCMs). ${ }^{26}$ The dielectric constant of $\mathrm{SiO}_{2}$ was taken to be 2.09. Periodic boundary condition (under normal incidence) or Bloch boundary condition (under oblique incidence) were used in the SGG plane, and perfectly matched layer (PML) boundary condition was chosen normal to the SGG plane. A linearpolarized plane wave in the range of $1.0-1.6 \mu \mathrm{~m}$ was selected as the light source.

Figure 3 shows the simulated transmission spectra and extinction ratio of SGG polarizer fabricated on InP, as a function of wavelength and pitch. When the pitch is larger than $500 \mathrm{~nm}, \mathrm{TE}$ transmission (Figure 3b) is just over 20\%, indicating a poor polarization performance. Although TE transmission is suppressed for the pitches below 500 nm (Figure 3b), a low TM transmission in the same area (Figure 3a) is also observed in the range of $1.0-1.6 \mu \mathrm{~m}$, resulting in low extinction ratio in Figure 3c.

It is understood that the dark area in Figure 3a is caused by propagating surface plasmonic polariton (SPP). As a SPP wave propagates at the interface, wave vector conservation is provided by diffraction on a periodic structure. ${ }^{27}$


Figure 3. Simulated normal incident transmission spectra of $\mathrm{Au} / \mathrm{InP}$ structure, as a function of wavelength and pitch: (a) TM polarized incident light, (b) TE polarized incident light, and (c) extinction ratio, as defined by TM/TE. The red dotted line in panel a presents the SPP resonance ( $i=$ $\pm 1, j=0)$ in the $\mathrm{Au} / \mathrm{InP}$ interface.

$$
\begin{equation*}
\mathbf{k}_{\mathrm{SP}}=\mathbf{k}_{0} \sin \theta \pm i\left(\frac{2 \pi}{D_{x}}\right) \mathbf{u}_{x} \pm j\left(\frac{2 \pi}{D_{y}}\right) \mathbf{u}_{y} \tag{1}
\end{equation*}
$$

where $\mathbf{K}_{\mathrm{sp}}$ is the SP wavevector, $\mathbf{K}_{0}$ is the wavevector of light in vaccine, $\theta$ is the angle of incidence, $D_{x, y}$ is the periodicity of the structured film in the $x$ - and $y$-directions, $\mathbf{u}_{x}$ and $\mathbf{u}_{y}$ are the reciprocal lattice vector, and $i$ and $j$ are integer numbers corresponding to different directions of SPP. In addition, the magnitude of SP wave vector is given by

$$
\begin{equation*}
\left|\mathbf{K}_{\mathrm{SP}}\right|=\frac{2 \pi}{\lambda} \sqrt{\frac{\varepsilon_{\mathrm{m}} \varepsilon_{\mathrm{d}}}{\varepsilon_{\mathrm{m}}+\varepsilon_{\mathrm{d}}}} \tag{2}
\end{equation*}
$$

where $\lambda$ is the wavelength of incident light, $\varepsilon_{\mathrm{m}}$ the permittivity of metal, and $\varepsilon_{\mathrm{d}}$ the permittivity of the adjacent medium.

For normal incidence of light onto an SGG, using eqs 1 and 2, the SPP resonance wavelength is obtained:

$$
\begin{equation*}
\lambda_{\mathrm{SPP}}=\frac{D}{\sqrt{i^{2}+j^{2}}} \sqrt{\frac{\varepsilon_{\mathrm{m}} \varepsilon_{\mathrm{d}}}{\varepsilon_{\mathrm{m}}+\varepsilon_{\mathrm{d}}}} \tag{3}
\end{equation*}
$$

which depicts the relationship between the SPP wavelength $\left(\lambda_{\text {SPP }}\right)$ and the grating pitch $(D)$ in the $\mathrm{Au} / \mathrm{InP}$ interface for $i=$ $\pm 1, j=0$, as shown by the red dotted line in Figure 3a, proving that the dark area is truly caused by SPP resonance. Figure 4 presents simulated and measured transmission spectra in the range of $1.0-1.6 \mu \mathrm{~m}$ for a fixed pitch of 400 nm , both of which show that the light in the $1.3-1.44 \mu \mathrm{~m}$ range is not polarized.


Figure 4. Simulated and measured transmission spectra of $\mathrm{Au} / \mathrm{InP}$ structure with pitch $=400 \mathrm{~nm}$, gold thickness $=100 \mathrm{~nm}$, and duty cycle $=0.5$ : (a) simulated transmission spectra and (b) measured transmission spectra.

Some deviations between measured and calculated value may be ascribed to the specific geometric parameters of the fabricated SGG polarizer.

Figure 5 presents both the simulated and measured transmission with different incidence angles at 1342 nm ,


Figure 5. Simulated and measured angle-resolved transmission spectra of $\mathrm{Au} / \mathrm{InP}$ structure for the wavelength at 1342 nm : (a) simulated transmission spectra and (b) measured transmission spectra.
which is close to the minimum of TM transmission. Both theoretical and experimental transmittances show unpolarization behavior for the angle between $\pm 8^{\circ}$. According to eq 1 , the SPP excitation is strongly related to the incident angle $\theta$. With the increasing of incident angle, SPP resonance disappears, leading to the increase of TM transmission. Although polarization begins to play with larger oblique incidence angles, the incident light intensity decreases, resulting in low detection efficiency.

Figure 6 presents the electric field distribution and Poynting vectors of TM mode with normal incidence (Figure 6a), as well as oblique incidence at $30^{\circ}$ (Figure 6b) at $1.35 \mu \mathrm{~m}$. For normal incidence, a strong reflection of light can be clearly seen in the $E^{2}$ distribution, stemming from SPP mode, as discussed above. This is consistent with the power flow described by the simulated Poynting vector distribution in Figure 6a (i.e., negligible power flows through the InP substrate). However, for the oblique incidence in Figure 6b, SPP resonance disappears, leading to nonzero power flow into InP.

The existence of unpolarized area due to SPP mode in the concerned wavelengths significantly impairs the extinction quality of our polarizers. In order to eliminate the unwanted SPP modes in $1.0-1.6 \mu \mathrm{~m}$ with an SGG as a polarizer on InP, a


Figure 6. Electric field distributions and Poynting vectors of TM mode in $\mathrm{Au} / \mathrm{InP}$ structure at 1350 nm wavelength: (a) incident angle $=0^{\circ}$ and (b) incident angle $=30^{\circ}$.


Figure 7. Simulated normal incident transmission spectra of $\mathrm{Au} / \mathrm{SiO}_{2} / \mathrm{InP}$ structure, as a function of wavelength and pitch: (a) TM polarized incident light, (b) TE polarized incident light, and (c) extinction ratio, as defined by TM/TE.
dielectric layer with lower permittivity $\varepsilon_{\mathrm{d}}$ should be plugged into the interface between gold and $\operatorname{InP}$ (eq 2). In this work, a 200 nm SiO 2 film with $\varepsilon_{\mathrm{d}}=2.09$ is selected. Such a $\mathrm{SiO}_{2}$ layer not only moves the SPP mode out of the $1.0-1.6 \mu \mathrm{~m}$, but also acts as an antireflection layer, as will be discussed later.

SGG Polarizer on $\mathrm{SiO}_{2} / \mathrm{lnP}$. As mentioned above, an efficient way to eliminate the SPP mode in the sensing region of $1.0-1.6 \mu \mathrm{~m}$ is to add a $\mathrm{SiO}_{2}$ layer between gold and InP to form a $\mathrm{Au} / \mathrm{SiO}_{2} / \mathrm{InP}$ sandwich structure. Figure 7 presents the transmission and extinction ratios of a $\mathrm{Au} / \mathrm{SiO}_{2} / \mathrm{InP}$ structure with a $\mathrm{SiO}_{2}$ thickness of 200 nm . The dark area in TM transmission has disappeared (Figure 7a) and lower TE transmission is presented (Figure 7b), resulting in significantly improved polarization performance over the $\mathrm{Au} / \mathrm{InP}$ structure (Figure 7c).

Figure 8 presents both the simulated and measured TM mode transmission for a specific grating pitch of 400 nm . Clear polarization is observed in the entire region of $1.0-1.6 \mu \mathrm{~m}$. The


Figure 8. Simulated and measured transmission spectra of a $\mathrm{Au} / \mathrm{SiO}_{2} /$ InP structure with pitch $=400 \mathrm{~nm}, \mathrm{SiO}_{2}$ thickness $=200 \mathrm{~nm}$, and duty cycle $=0.5$ : (a) simulated transmission spectra and (b) measured transmission spectra. The TM transmission dip at 1350 nm is totally removed.
simulated transmittance is quantitatively in good agreement with the measured value, indicating that the $\mathrm{SiO}_{2}$ in the $\mathrm{Au} / \mathrm{InP}$ interface is essential for the SGG to be a polarizer on the InP substrate.

With such an SGG/ $\mathrm{SiO}_{2} / \mathrm{InP}$ trilayer, the permittivity of the media around the gold grating is changed from 10.2 (InP at $1350 \mathrm{~nm})$ to $2.1\left(\mathrm{SiO}_{2}\right)$, shifting the resonance wavelength from 1350 nm to 650 nm (see eq 2). Moreover, the $\mathrm{SiO}_{2}$ layer can play a role of an antireflection layer to improve the quantum efficiency of the InGaAs sensor. Therefore, the $\mathrm{Au} /$ $\mathrm{SiO}_{2} / \mathrm{InP}$ structure should be a reasonable choice for the polarizer in InP-based InGaAs sensors in the range of $1.0-1.6$ $\mu \mathrm{m}$.

To further study the transmission process of TM mode, both the electric field distribution and Poynting vectors were calculated for the $\mathrm{Au} / \mathrm{SiO}_{2} / \mathrm{InP}$ structure, as shown in Figure 9. Poynting vector plot also illustrates enhanced power flow


Figure 9. TM mode in a $\mathrm{Au} / \mathrm{SiO}_{2} / \mathrm{InP}$ structure at 1350 nm : (a) electric field distribution and (b) Poynting vector distribution.
into the InP substrate. In our case, there are two types of resonance mechanisms: (i) SPP resonance (horizontal surfaceplasmon resonance) in the $\mathrm{Au} / \mathrm{InP}$ interface, and (ii) localized cavity mode (vertical surface-plasmon resonance) located in the slits. ${ }^{28,29}$ In the $\mathrm{Au} / \mathrm{InP}$ structure, SPP resonance is the dominant mechanism. The horizontal SPP reduces the transmission, as shown in Figure 3, by either reflecting some of the light or converting into Joule loss in the substrate. By adding a layer of $\mathrm{SiO}_{2}$ to the interface of $\mathrm{Au} / \mathrm{InP}$, the horizontal SPP is eliminated, to reduce the reflectance. Consequently, the transmission is increased via the localized cavity mode, as shown by the very strong electric field and Poynting vectors in the slits in Figure 9.

Furthermore, the thickness of $\mathrm{SiO}_{2}$ should be carefully selected to maximize the transmission. Figure 10 presents the calculated TM transmission at various $\mathrm{SiO}_{2}$ thicknesses from 100 nm to 600 nm . It can be seen that the transmission can vary by $40 \%$ at $1.35 \mu \mathrm{~m}$ for different thicknesses. Using the transmission result in Figure 10 as a guide, the thickness of $\mathrm{SiO}_{2}$ should be designed according to the specific working wavelengths of the InGaAs sensor. Particularly for the interested wavelength of $1.35 \mu \mathrm{~m}$, a thickness of 100 nm should be used.

## 4. CONCLUSION

This paper investigates the feasibility of subwavelength metallic gratings as polarizers in short-wave infrared wavelengths for InP-based InGaAs sensors. $\mathrm{Au} / \operatorname{InP}$ and $\mathrm{Au} / \mathrm{SiO}_{2} / \mathrm{InP}$ structures were compared by FDTD simulation and optical characterizations. The $\mathrm{Au} / \mathrm{InP}$ structure shows a large TM transmittance dip with no polarization for the grating pitch


Figure 10. Calculated TM transmission spectra of the $\mathrm{Au} / \mathrm{SiO}_{2} / \mathrm{InP}$ structure as a function of $\mathrm{SiO}_{2}$ thickness in the range of $100-600 \mathrm{~nm}$.
from 200 nm to 500 nm . The low TM transmission in this structure has been explained by the existence of SPP resonance in the $\mathrm{Au} / \mathrm{InP}$ interface. However, the $\mathrm{Au} / \mathrm{SiO}_{2} / \mathrm{InP}$ structure has demonstrated a stable TM transmission and extinction ratio in the entire sensing wavelength. Polarizers with such a sandwich structure have been successfully fabricated and its polarization capability has been demonstrated by optical characterization. Besides, the added $\mathrm{SiO}_{2}$ layer should be beneficial to the transmission improvement as an antireflection layer. This work sheds lights on further development of integrated polarimetric sensors in short-wave infrared region. Further work in the selection of metal materials, as well as optimization of the pitch and duty cycle, should be carried out for improving the polarization performance.

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## Author Contributions

The manuscript was written through contributions of all authors. All authors have given approval to the final version of the manuscript.

## Notes

The authors declare no competing financial interest.

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